

3.2 ‘Novel Serial Elastic Actuator Elastic module without friction hysteresis’ (MD-T-02)

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Abstract

A serial elastic actuator (SEA) includes a physical compliance. Thereby the actuator provides the following characteristics: sensible for external mechanical impacts, decoupling loads from the motor side, low-pass filter behavior for loads and it stores energy. This characteristics privilege the actuator for applications with a direct human-robot contact like industrial, rehabilitation or teleoperation scenarios and for walking robots. The talk gives an overview of common applications and designs. It gives a more detailed view on SEA-development at the DFKI project ‘Cario’. Generally the implementation of a compliance cause hysteresis problems by friction or material characteristics. Depending of the positioning of elasticity it complicates the design development and increases the actuator size. To solve these problems a customized torsional disc spring is implemented in a serial elastic actuator module. The iterative spring design workflow from the CAD model to the large displacement FEM simulation is described. The DFKI design of a serial elastic module for a 5 Nm actuator is shown beside other research designs.



Novel Serial Elastic Actuator

Elastic module without friction hysteresis

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25.06.2015

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Outline



- SEA Motivation
- SEA Applications
- Design of SEAs
- Capio SEA, Design and Usage
- Novel SEA Module, Design and Dimensioning
- Next Steps and Future Work
- References



SEA Motivation



- Robot safety principles
 - Supervision, force control, lightweight
 - ISO 13482, ISO 10218
 - Inherent safe design → SEA
- Robot industrial application
 - Usually robot human interaction with safety distance
 - Dangerous situation by robot motion
 - New: robot as cooperative partner in direct contact
- Robot rehabilitation application
 - Direct human robots contact
 - Unhealthy operator/patient

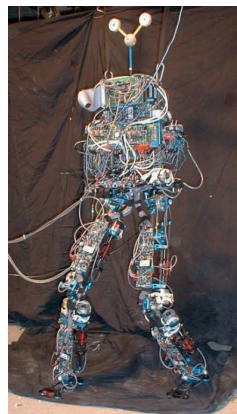
SEA Applications



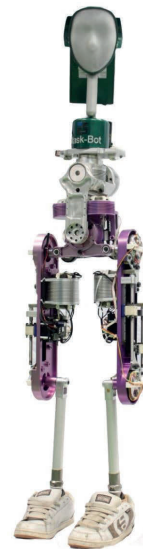
- Mostly used for legged robots
- No commercial actuators available
- Few industrial application



Baxter

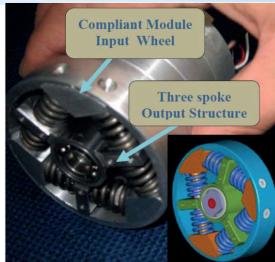


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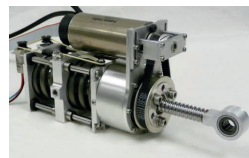


Herbert

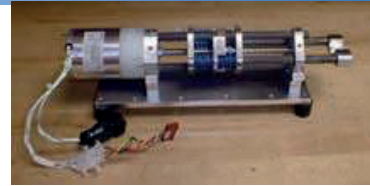
Designs of SEAs



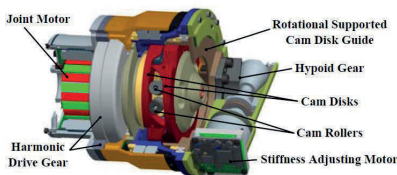
Tsagarakis 2009



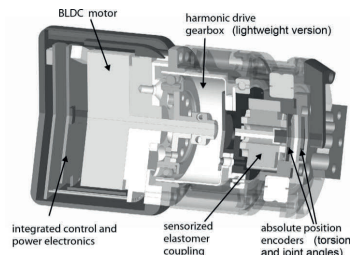
Paine 2012



Pratt 1995



Wolf 2011

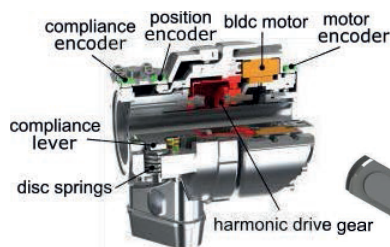


Paskarbeit 2013

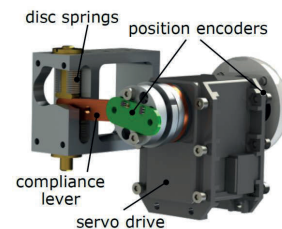
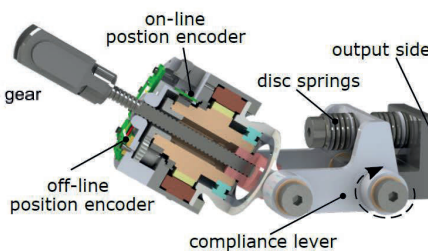
Capio SEAs at the RIC



- Nominal torque 60 Nm
- Overall weight 1kg
- Robodrive ILM 70 x 10, 370 W, 3500 rpm, 1.25 Nm
- Harmonic Drive CPL 20, ratio 1:80
- Variable set of disc springs



- Maximum force 790 N
- 166 mm/s max. travel velocity
- Overall weight 320 g
- Robodrive ILM 50x10, 140 W, 5000 rpm, 0.28 Nm
- Driven nut, Spindle 2 mm lead
- Offline tooth wheel nonius with iC-Haus MH 12 bit sensors
- Online iC-Haus MU 19 bit sensor for BLDC commutation and travel
- Compliance via structure
- Variable set of disc springs

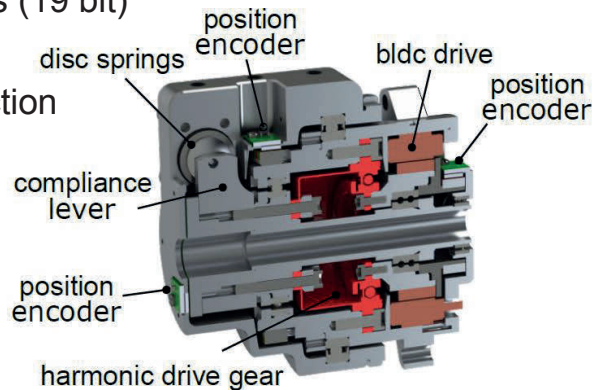
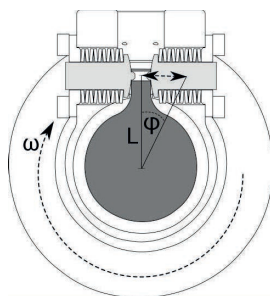


- Dynamixel 24F, 2.6 Nm torque at 12 V, 126 rpm
- Compliance via structure
- Variable set of disc springs
- Compliance measured with two iC-Haus MH sensors

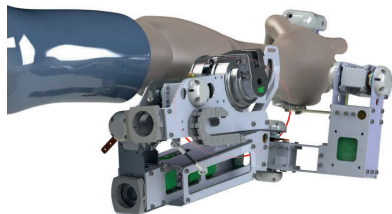
Capio Design 14 / 28 Nm



- ILM 50x8 robodrive and CPL 14 - 50/100 harmonic drive
- 28 Nm, 140 W, 600g
- 3 x iC-Haus MU sensors (19 bit)
- Variable disc springs
- Hysteresis by spring friction



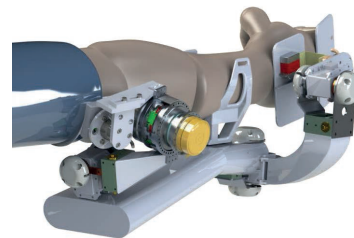
Usage at the Capio Exoskeleton



Current forearm setup

- Current setting for internal/external rotation of upper arm and elbow extension/flexion: Capio SEA 14 Nm
- Weight 4 x 600 g =2400 g
- Experimental evaluation showed a max required torque of 4 Nm

- Development of adapted torque SEA for weight reduction and safety aspects
- Expected weight reduction about 1000 g



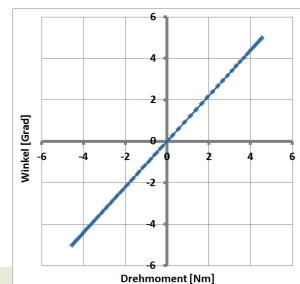
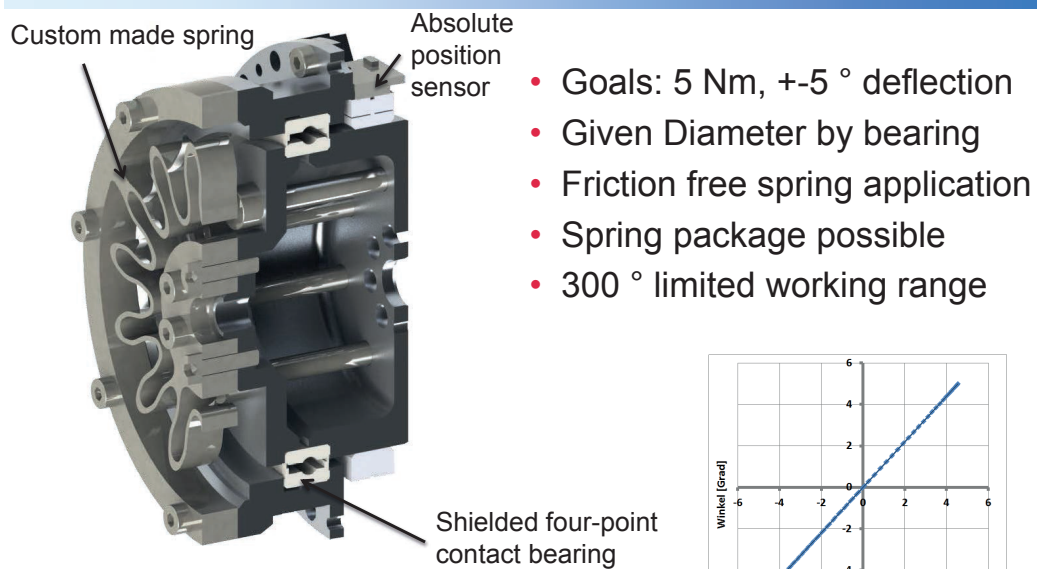
Sketch of new forearm setup

Known SEA Problems



- Hysteresis by spring contact friction
- Hysteresis by elastomer compliant element (nonlinear material characteristics)
- Hysteresis by friction in a sealed bearing
- Short lever arm design if inside housing
- Expensive milled parts necessary
- Clunking and moving of unloaded springs
- Not all torques possible with commercial springs


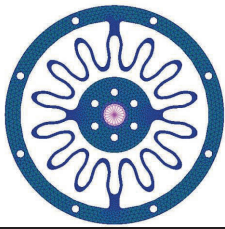
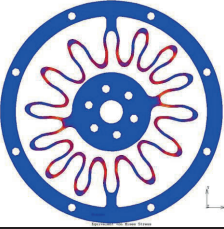
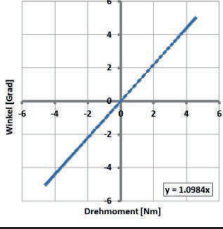
Serial Elastic Modul



Spring Dimensioning Workflow

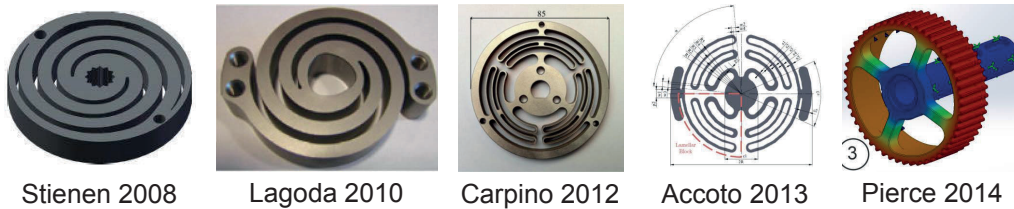


- Goals: 5 Nm and +5 ° deflection
- Iterative process, morphological adaption for stress reduction

CAD-Design Solidworks	Mesh-Design Patran/Nastran	FEM-Simulation Marc/Mentat	Evaluation
			
Parametric Design	2D- simplification TRIA-Elements	Large-Displacement Simulation	Spring-Stiffness Calculation



Custom Rotative Spring Designs



Stienen 2008

Lagoda 2010

Carpino 2012

Accoto 2013

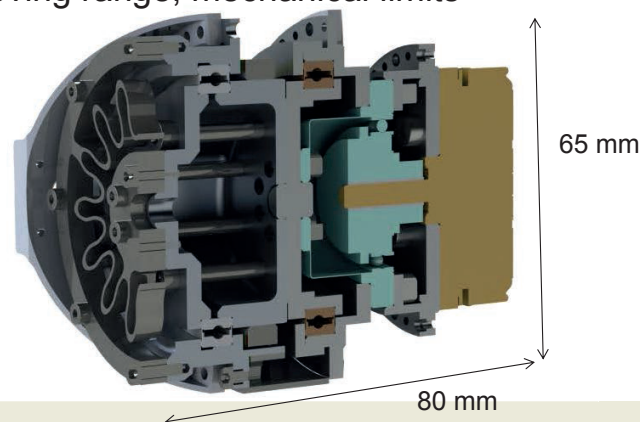
Pierce 2014

Year	Name	Stiffness [Nm/rad]	Max Torque [Nm]	Max Deflection [rad]	Outer Diameter [mm]	Thickness [mm]	Weight [g]
2008	Stienen	88,00	22,00	0,25	50,00	10,00	-
2010	Lagoda	219,00	90,00	0,50	~90	-	-
2012	Carpino	98,00	7,68	0,08	85,00	3,00	61,50
2013	Accoto	272,25	30,00	0,11	90,00	23,50	370,00

Serial elastic actuator



- Base: Limes Actuator 5 Nm, Maxon EC flat 45, HFUC11–50
- Module weight 160 g, Overall weight 380 g
- One iC-Haus MU target (19 bit) for deflection and position
- 300 ° moving range, mechanical limits



Next Steps and Future Work



- Assemble joint, integrate in testbed and Capio forearm
- Spring design
 - Evaluation spring characteristics
 - Optimize design concerning stress, size, weight of spring
 - Safety limits for deflection angle
- Module design
 - Implement strain gauge at spring for redundant torque signal or removing iC-Haus MU sensor
 - Compact design and weight reduction
 - Implement brakes on motor side

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Thank you!

Question?

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